



Test description

Support is made of no-tension springs. A horizontal force F is applied on the top-right node of a concrete block made of plateshell elements; self weight of each plate-shell element is applied as nodal loads on element nodes. When F is null, all the springs are in compression under self weight. Increasing F, compression in the springs on the right decreases until compression is equal to zero, then they stop to work. When a critical value of F is reached there is no more equilibrium. In this test a force equal to W/6 is applied to the block, so springs reaction should coincide to the diagram in the figure on the right.

Test model: curanSP_001.WSR



Springs properties							
	k ₁	Dy	k ₂	D _u	Law	Gap	Dy F
l	1500N/mm	500mm	1000N/mm	∞	no tension	Omm	X
	Note: exter	nal springs	have the for	llowing stif	fnesses: k ₁ /	2 and $k_2/2$	- k2 ***

Concrete properties (plate-shell elements)						
ρ	E	ν	Fy	Ft		
$2,5e-05N/mm^{3}$	25491N/mm ²	0,2	20N/mm^2	20N/mm ²		

Geometry and loads						
Sides	Mesh	Elements thickness	Weight	Force		
L = 5000 mm	10x10 elements	150mm	W = 93750N	F = W/6		

CHECK

Internal force in each spring should be equal to: $-2*W/L*(x_i/L)*Lx_i$ where x_i is the position of the spring 'i' and L_{x_i} is the length associated to that spring. As check, axial forces computed by Curan in some springs were compared with hand computations according to the previous formula. Springs numbering is reported. Note that L_x of external springs is half of L_x of internal ones.

19876549240

Load case	Value	Unit	CURAN	THEORETICAL	% diff.
1	Spring #5 axial force	Ν	-9,374E+03	-9,375E+03	-0,02
1	Spring #9 axial force	Ν	-1,489E+04	-1,500E+04	-0,76
1	Spring #11 axial force	Ν	-9,290E+03	-9,141E+03	1,64

% difference = (CURAN - THEORETICAL) / THEORETICAL * 100

Precision of limit multiplier for the analysis: 0.005